

THREAD FORMULA

METRIC 60° (M)		
$H = 0,86603 \cdot P$ $h_3 = 0,61343 \cdot P$ $d_2 = d - (0,6495 \cdot P)$ $d_3 = d - (2 \cdot h_3)$ $r = \frac{H}{6} = 0,14434 \cdot P$		<p>To find the correct drill diameter for internal threads subtract the pitch (P) from the outside diameter (d).</p> <p>i.e. drill for M16x2 = 14.0mm</p>

UNIFIED INCH 60° (UNC, UNF, UNR, NPS)		
$H = 0,86603 \cdot P$ $h_3 = 0,61343 \cdot P$ $d_2 = d - (0,6495 \cdot P)$ $d_3 = d - (2 \cdot h_3)$ $r_1 = 0,10825 \cdot P$ $r_2 = 0,1443 \cdot P$		<p>Pitch (P) is 1 divided by the number of threads per inch (TPI)</p>

WHITWORTH 55° (BSW, BSF, G)		
$H = 0,96049 \cdot P$ $h_3 = 0,64033 \cdot P$ $d_2 = d - h_3$ $d_3 = d - (2 \cdot h_3)$ $r = 0,13733 \cdot P$		<p>Pitch (P) is 1 divided by the number of threads per inch (TPI)</p>

American Taper NPT	Whitworth BSPT (R, Rc)
<p>NPT uses the following TPI:</p> <p>27, 18, 14, 11½ and 8</p>	<p>BSPT uses the following TPI:</p> <p>28, 19, 14 and 11</p>

N.B. The same TPIs apply also to NP and Whitworth (G) straight/parallel pipe threads

ACME 29°		
$H = 1,933 \cdot P$ $H_1 = 0,5 \cdot P$ $H_4 = 0,5 \cdot P + a = H_1 + a$ $h_3 = 0,5 \cdot P + b = H_1 + b$ $z = 0,25 \cdot P$ $D_4 = d + 2a$ $d_3 = d - 2 h_3$ $d_2 = D_2 = d - 2z$		<p>Pitch (P) is 1 divided by the number of threads per inch (TPI)</p>

STUB ACME 29°		
$H = 1,933 \cdot P$ $H_1 = 0,3 \cdot P$ $H_4 = 0,3 \cdot P + a = H_1 + a$ $h_3 = 0,3 \cdot P + b = H_1 + b$ $z = 0,15 \cdot P$ $D_4 = d + 2a$ $d_3 = d - 2 h_3$ $d_2 = D_2 = d - 2z = d - 0,3 \cdot P$		<p>Pitch (P) is 1 divided by the number of threads per inch (TPI)</p>

METRIC TRAPEZOID 30° (Tr)		
$H = 1,866 \cdot P$ $H_1 = 0,5 \cdot P$ $H_4 = 0,5 \cdot P + ac$ $h_3 = 0,5 \cdot P + b$ $z = 0,25 \cdot P$ $D_4 = d + 2ac$ $d_3 = d - 2h_3$ $d_2 = D_2 = d - 2z$		

METRIC TRAPEZOID STUB 30°		
$H = 1,866 \cdot P$ $H_1 = 0,3 \cdot P$ $H_4 = 0,3 \cdot P + a = H_1 + a$ $h_3 = 0,3 \cdot P + b = H_1 + b$ $z = 0,15 \cdot P$ $D_4 = d + 2a$ $d_3 = d - 2h_3$ $d_2 = D_2 = d - 2z$ $= d - 0,3 \cdot P$		